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ITEM NO.	NO. DATE COPIES DESCRIPTION  1 6/16 1 Preliminary Report on Site Hydrogeology								
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September 24, 1987

K-0971-2

Mapco Alaska Petroleum, Inc. 1100 H&H Lane North Pole, Alaska 99705

Attention: Ms. Kathleen McCullom

RE: EVALUATION OF GROUNDWATER FLOW, NORTH POLE REFINERY

Dear Ms. McCullom:

This letter presents the results of our recent evaluation of groundwater flow at the North Pole Refinery. This work was conducted in general accordance with our proposal to you dated September 10, 1987. The purpose of this work was to further investigate groundwater flow at the site, specifically with reference to vertical gradients at the north of the site and flow along the railroad spur.

#### Scope of Work

On September 14 and 15, 1987 one new monitoring well and four new sampling wells were installed at the site. On September 16, 1987 water levels were read in 19 recovery wells, 40 sampling, monitoring, and other wells, and 3 gravel pits on site. A survey of these points for elevation and horizontal location was performed by Design Alaska on September 16 through 19, 1987. Note that the recovery wells which were also surveyed in February, 1987 had heaved as much as 0.06 feet or settled as much as -0.06 feet since then. All but one of the S-series wells had heave, as much as 0.31 feet.

Table 1 presents the surveyed elevations of the wells used in this study. Table 2 presents the horizontal locations of these wells referenced to the refinery's coordinate system. Figure 1 is a plot plan of the well locations.

Water level measurements were made by John Cronin of our firm and Kathleen McCullom of Mapco. Water levels in the eight MW-series monitoring wells were measured with an electric water level sounder. A steel tape measure with water finding paste was used to measure depth to water (and depth to product, where applicable) in all other wells. Tables 3 through 10 present measured and calculated water/product level data. During the course of the measurements, the water table was dropping at the rate of 0.01 feet per 2 hours. The calculated potentiometric surface elevations were later corrected for this change before using them to plot groundwater surface contours.

Figure 2 is a contour plot of the potentiometric surface (the water table corrected for the presence of floating hydrocarbons in any wells) on September 16, 1987. This plot indicates the same general groundwater flow direction of about North 10° West which has been previously concluded from other data. However, the inclusion of the elevations of the three gravel pits on the plot reveals some of the localized differences in flow direction which exist at the site. On Figure 2, arrows have been drawn, at right angles to the water table contours, which indicate our inferred direction of groundwater movement. These arrows show that, superimposed upon the northerly regional gradient, there is flow into the south sides and out of the north sides of the gravel pits. This can also be seen in the 3-dimensional isometric plot of the water table surface presented in Figure 3.

It should be noted that all contour plots in this report were produced by a computer program using a Kriging algorithm. This results in some inevitable approximations and smoothing of the data. The scarcity of real data in some areas of the plots, particularly in the southwest corner, results in calculated data which, while they may be arithmetically correct, may not portray reality. In addition, the water levels plotted at the north end of the site are a mix of levels above and below permafrost. The plots have been included for visualization, and should be viewed in light of the cautions expressed above.

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#### Discussion

Figure 2 indicates that on September 16, 1987 the general direction of groundwater flow at the site was about North 10° West. The overall gradient, measured from well S-19 to S-9, is 5.1 feet per mile. The gradient appears to flatten across the site to the north, from 6 feet per mile or greater at the south end to 4 feet per mile or less at the north end. This flattening may be due to the presence of permafrost north of the site, or may be a natural function of increasing distance from the Tanana River, which is recharging the aquifer.

For comparison, Figure 4 presents potentiometric surface contours based on February 4, 1987 measurements of only the S-series wells. These data indicate the same general direction of groundwater flow, and a slightly lower overall gradient (about 4.8 feet per mile from S-19 to S-9).

The installation of a shallow piezometer (S-25) adjacent to the Truck Rack Water Well (#4) allows vertical gradients to be examined at this location. In addition, surveyed elevations on the MW-series wells allows vertical gradients to be examined to the north and south of the refinery as well. Given an adjacent deep well and shallow well, a higher water level in the shallow well indicates the potential for downward water flow, and a higher water table in the deeper well indicates the potential for upward water flow. Note the indication of the "potential" for vertical flow. For instance, the MW-102/MW-103 pair are below and above a permafrost layer, which will not allow vertical flow. Tabulated below are the measured head differences, and the inferred direction of vertical groundwater flow, based on all available measurements from these well pairs.

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	MW-101	MW-102	MW-105	Truck Rack
Well Pair	MW-101A	MW-103	MW-105A	S-25
Date		Head Difference	e in Feet	
4/7/87	.52	.26	.17	NA
	(up)	(up)	(up)	
5/6/87	.01	.53	.03	NA
	(down)	(up)	(down)	
8/26/87	.01	.65	.20	NA
	(up)	(up)	(up)	***
9/16/87	0	.17	.17	.02
		(down)	(up)	(down)

In our opinion, the measured head differences of only a few hundredths of a foot probably represent the limit of accuracy of the measurements, and most likely indicate no significant vertical flow. Thus no vertical flow is apparent at the Truck Rack Well.

MW-102 and MW-103 are about 200 feet apart, and thus some difference would be expected between these two wells. However, the change in magnitude of head difference and inferred direction indicates some change in the hydrology in this area during the year.

The two true pairs, MW-101/MW-101A and MW-105/MW-105A, generally indicate the potential for some upward flow. This may be the result of recharge from the Tanana River and/or permeability differences with depth in the formation.

The new piezometer installed along the railroad spur, S-26, confirms the existence of a gradient to the northeast along the spur. This gradient,

# WATER/PRODUCT LEVEL DATA

PROJECT LOCATION: NORTH POLE REFINERY

RECORDED BY: K. McCULLOM

DATE: SEPTEMBER 16, 1987

WELL NO.	TIME	CASING RIM ELEVATION (FEET)	TAPE READING AT RIM	TAPE READING AT PRODUCT	TAPE READING AT WATER	DEPTH TO WATER FEET)	WATER SURFACE ELEVATION (FEET)	PRODUCT THICKNESS (FEET)	POTENTIOME SURFACE ELEVATION (FEET)	COMMENTS
15 18	1550 1605	496.68 498.65	11.00 13.00	0.40	0.16	10.84	485.84 485.96	0.24	486.03 486.13	R-13 R-18

TABLE 4

# WATER/PRODUCT LEVEL DATA

PROJECT LOCATION: NORTH POLE REFINERY

RECORDED BY: K. McCULLOM / J. CRONIN

DATE: SEPTEMBER 16, 1987

WELL NO.	TIME	CASING RIM ELEVATION (FEET)	TAPE READING AT RIM	TAPE READING AT PRODUCT	TAPE READING AT WATER		WATER SURFACE ELEVATION (FEET)	PRODUCT THICKNESS (FEET)	POTENTIOME SURFACE ELEVATION (FEET)		OMMENTS	
1	1555	493.98	9.00	0.54	0.29	8.71	485.27	0.25	485.47	R-1		
3	1300	493.99	7.50	0.88	0.40	7.10	486.89	0.48	487.28	R-3		
8	1330	495.19	9.65	0.50	0.00	9.65	485.54	0.50	485.95	R-7	NO WATER	IN HOLE BE
9	1335	494.40	9.65	1.16	0.00	9.65	484.75	1.16	485.69	R-8	NO WATER	IN HOLE BE
10	1545	494.09	9.01	1.21	0.30	8.71	485.38	0.91	486.12	R-9		
19	1607	498.08	14.50	3.26	0.11	14.39	483.69	3.15	486.24	R-19		
20	1615	499.10	15.30	3.10	0.35	14.95	484.15	2.75	486.38	R-20		
39	1620	497.88	14.90	4.02	0.31	14.59	483.29	3.71	486.30	S-20		
41	1635	497.79	14.50	3.83	0.54	13.96	483.83	3.29	486.49	S-22		

# WATER/PRODUCT LEVEL DATA

PROJECT LOCATION: NORTH POLE REFINERY RECORDED BY: K. McCULLOM

DATE: SEPTEMBER 16, 1987

WELL NO.	TIME	CASING RIM ELEVATION (FEET)	TAPE READING AT RIM	TAPE READING AT PRODUCT	TAPE READING AT WATER	DEPTH TO WATER (FEET)	WATER SURFACE ELEVATION (FEET)	PRODUCT THICKNESS (FEET)	POTENTIOME SURFACE ELEVATION (FEET)	TRIC COMMENTS
2	1255	494.01	7.50	0.68	0.45	7.05	486.96	0.23	487.15	R-2
4	1200	494.59	8.00	0.59	0.39	7.61	486.98	0.20	487.14	R-4
11	1410	495.00	9.50	0.91	0.50	9.00	486.00	0.41	486.34	R-10
12	1415	492.78	7.00	0.61	0.22	5.78	486.00	0.39	486.32	R-10A
13	1400	495.02	9.50	0.88	0.45	9.05	485.97	0.43	486.32	R-11

# WATER/PRODUCT LEVEL DATA

PROJECT LOCATION: NORTH POLE REFINERY

RECORDED BY: K. McCULLOM

DATE: SEPTEMBER 16, 1987

WELL NO.	TIME	CASING RIM ELEVATION (FEET)	TAPE READING AT RIM	TAPE READING AT PRODUCT	TAPE READING AT WATER		WATER SURFACE ELEVATION (FEET)	PRODUCT THICKNESS (FEET)	POTENTIOMET SURFACE ELEVATION (FEET)	COMMENTS
14	1420	493.81	8.50	0.96	0.33	8.17	485.64	0.63	486.16	R-12

# WATER/PRODUCT LEVEL DATA

PROJECT LOCATION: NORTH POLE REFINERY

RECORDED BY: K. McCULLOM

DATE: SEPTEMBER 16, 1987

WELL NO.	TIME	CASING RIM ELEVATION (FEET)	TAPE READING AT RIM	TAPE READING AT PRODUCT	TAPE READING AT WATER (	DEPTH TO WATER FEET)	WATER SURFACE ELEVATION (FEET)	PRODUCT THICKNESS (FEET)	POTENTIOME SURFACE ELEVATION (FEET)	COMMENTS
16 17	1445 1455	493.94 493.73	8.77 9.30	0.56 1.43	0.30	8.47 8.97	485.47 484.76	0.26	485.69 485.68	R-14 R-14A

## WATER/PRODUCT LEVEL DATA

PROJECT LOCATION: NORTH POLE REFINERY RECORDED BY: K. McCULLOM

DATE: SEPTEMBER 16, 1987

WELL NO.	TIME	CASING RIM ELEVATION (FEET)	TAPE READING AT RIM	TAPE READING AT PRODUCT	TAPE READING AT WATER (	DEPTH TO WATER FEET)	WATER SURFACE ELEVATION (FEET)	PRODUCT THICKNESS (FEET)	POTENTIOME SURFACE ELEVATION (FEET)	TRIC
5	1427	495.43	9.50	1.13	0.38	9.12	486.31	0.75	486.96	R-5
6	1435	496.68	10.50	0.70	0.59	9.91	486.77	0.11	486.86	R-5A

TABLE 9

# WATER/PRODUCT LEVEL DATA

PROJECT LOCATION: NORTH POLE REFINERY RECORDED BY: J. CRONIN/K. McCULLOM

DATE: SEPTEMBER 16, 1987

WELL		CASING RIM	TAPE READING	TAPE READING	TAPE READING	DEPTH TO	WATER SURFACE	PRODUCT	POTENTIOME SURFACE	TRIC
NO.	TIME	ELEVATION	AT RIM	AT PRODUCT	AT WATER	WATER	ELEVATION	THICKNESS	ELEVATION	COMMENTS
		(FEET)				FEET)	(FEET)	(FEET)	/ PPPT \	
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21	1556	494.16	6.80	0.00	0.15	6.65	487.51	0.00	487.51	S-1
22	1302	496.71	9.80	0.00	0.15	9.65	487.06	0.00	487.06	S-2A
23	1305	493.47	6.70	0.00	0.13	6.57	486.90	0.00	486.90	S-3
24	1316	495.45	9.10	0.00	0.13	8.97	486.48	0.00	486.48	S-4
25	1320	495.60	9.40	0.00	0.17	9.23	486.37	0.00	486.37	S-5
26	1325	492.30	6.30	0.00	0.13	6.17	486.13	0.00	486.13	S-6
27	1339	495.06	9.60	0.00	0.16	9.44	485.62	0.00	485.62	S-8
28	1333	493.97	8.40	0.00	0.12	8.28	485.69	0.00	485.69	S-8A
29	1400	496.10	10.80	0.00	0.11	10.69	485.41	0.00	485.41	S-9
30	1407	494.65	9.30	0.00	0.14	9.16	485.49	0.00	485.49	S-10
31	1412	497.23	11.70	0.00	0.16	11.54	485.69	0.00	485.69	S-11
32	1419	496.58	11.00	0.00	0.19	10.81	485.77	0.00	485.77	S-12 <
33	1431	496.21	10.50	0.00	0.17	10.33	485.88	0.00	485.88	S-13
34	1427	496.81	10.90	0.00	0.17	10.73	486.08	0.00	486.08	S-13A "
35	1531	496.80	10.80	0.00	0.12	10.68	486.12	0.00	486.12	S-14
36	1437	497.23	10.20	0.00	0.17	10.03	487.20	0.00	487.20	S-17 /
37	1545	498.30	10.60	0.00	0.13	10.47	487.83	0.00	487.83	S-18A
38	1549	495.43	7.70	0.00	0.12	7.58	487.85	0.00	487.85	S-19 L
42	1705	496.09	10.30	0.00	0.18	10.12	485.97	0.00	485.97	S-23/
43	1630	495.96	9.30	0.00	0.18	9.12	486.84	0.00	486.84	S-24 /
44	1212	497.06	11.50	0.00	0.15	11.34	485.72	0.00	485.72	S-25
45	1159	495.65	10.40	0.00	0.11	10.29	485.36	0.00	485.36	S-26

TABLE 10

## WATER/PRODUCT LEVEL DATA

PROJECT LOCATION: NORTH POLE REFINERY RECORDED BY: J. CRONIN

DATE: SEPTEMBER 16, 1987

WELL		CASING RIM	TAPE READING	TAPE READING	TAPE READING	DEPTH TO	WATER SURFACE	PRODUCT	POTENTIOME SURFACE	TRIC
NO.	TIME	ELEVATION (FEET)	AT RIM	AT PRODUCT	AT WATER	WATER (FEET)	ELEVATION (FEET)	THICKNESS (FEET)	ELEVATION (FEET)	COMMENTS
47	1445	494.77	8.10	0.00	0.16	7.94	486.83	0.00	486.83	CONSTRUCTION WELL
48 49	1349 1227	494.24	8.50	0.00	0.16	8.34	485.90 485.70	0.00	485.90 485.70	DISTRIBUTION WELL TRUCK RACK WELL
50	920	495.27	9.97	0.00	0.00	9.97	485.30	0.00	485.30-	411181 MW-101
51	922	493.26	7.96	0.00	0.00	7.96	485.30	0.00	485.30	MW-101A
52	1047	493.38	8.25	0.00	0.00	8.25	485.13	0.00	485.13	MW-102
53	1116	494.09	8.79	0.00	0.00	8.79	485.30	0.00	485.30	MW-103
54	1129	496.45	11.54	0.00	0.00	11.54	484.91	0.00	484.91	MW-104
55	951	497.50	9.43	0.00	0.00	9.43	488.07	0.00	488.07	MW-105A
56	953	497.85	9.61	0.00	0.00	9.61	488.24	0.00	488.24	MW-105
57	933	497.49	11.19	0.00	0.00	11.19	486.30	0.00	486.30	MW-106
58	1506	495.39	10.20	0.00	0.18	10.02	485.37	0.00	485.37	OM-1
59	1703	496.15	10.85	0.00	0.13	10.72	485.43	0.00	485.43	OM-2
60	1521	494.07	8.50	0.00	0.22	8.28	485.79	0.00	485.79	M-2
61	1451	492.83	6.30	0.00	0.12	6.18	486.65	0.00	486.65	M-3
62	1538	492.32	6.00	0.00	0.11	5.89	486.43	0.00	486.43	M-4
25	1642	495.60	9.40	0.00	0.15	9.25	486.35	0.00	486.35	S-5 CLOSURE
28	1645	493.97	8.40	0.00	0.10	8.30	485.67	0.00	485.67	S-8A CLOŞURE

